



SPACE PROPULSION TECHNOLOGY DIVISION



# MPD THRUSTER TECHNOLOGY

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SPACE PROPULSION TECHNOLOGY DIVISION



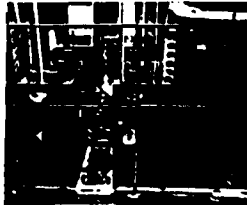
## IN-HOUSE PROGRAM OVERVIEW

- RE-ESTABLISHED IN 1987
- FOCUSED ON STEADY-STATE THRUSTERS AT POWERS  $< 1$  MW
- DEVELOPED PERFORMANCE MEASUREMENT AND DIAGNOSTICS TECHNOLOGIES FOR HIGH POWER THRUSTERS
- DEVELOPING MHD CODE
- GOALS ARE TO ESTABLISH
  - PERFORMANCE AND LIFE LIMITATIONS
  - INFLUENCE OF APPLIED FIELDS
  - PROPELLANT EFFECTS
  - SCALING LAWS

**MPD Thruster Technology**

**High Power MPD Thruster Test Stand**

**Power**



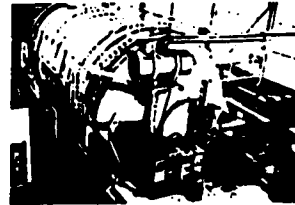
• 0.39 MW

**Thrust stand**



• 0.1 to 4 N

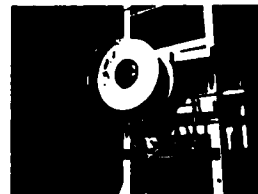
**Vacuum facility**



• 0.1 g/s at  $3 \times 10^{-4}$  TORR



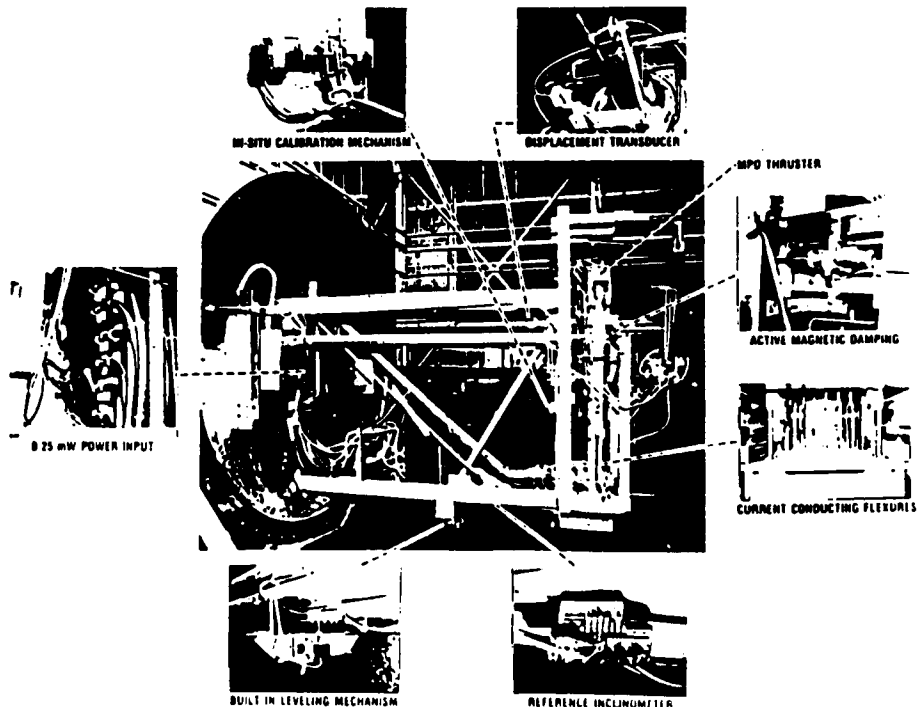
**Data/control**



**220 kW thruster**

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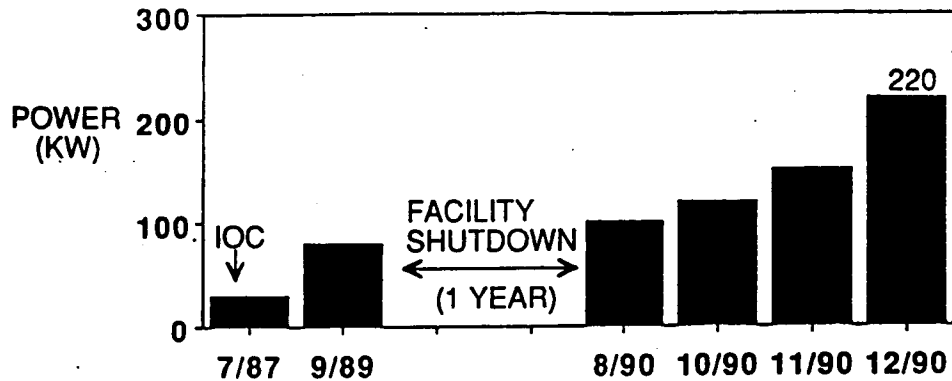
**MPD THRUSTER TEST STAND**



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HIGH POWER ELECTRIC PROPULSION (MPD)

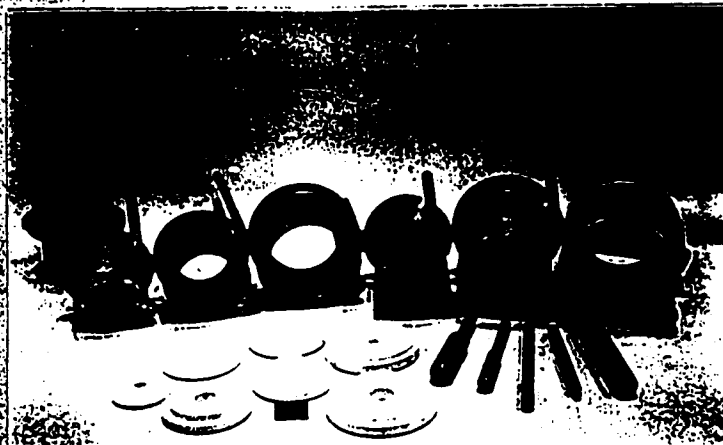
DEMONSTRATED MPD THRUSTER POWER



**DEMONSTRATED MPD THRUSTER POWER  
INCREASING RAPIDLY**

MPD Thruster Technology

Thruster Scaling and Materials Effects

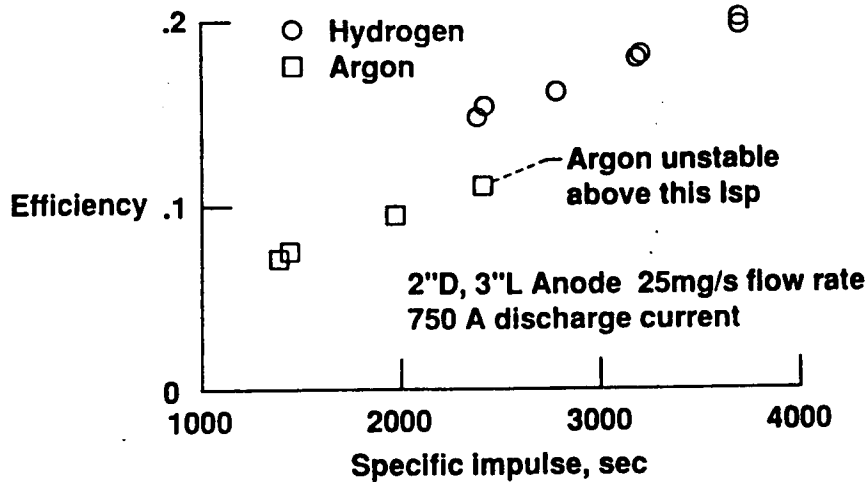


- 2, 3 and 4 inch diameter anodes both 3 and 6 inches long
- 0.5 and 1 inch diameter cathodes
- 2% Th and BaO impregnated tungsten cathodes

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MPD Thruster Technology

Performance Measured With Hydrogen and Argon



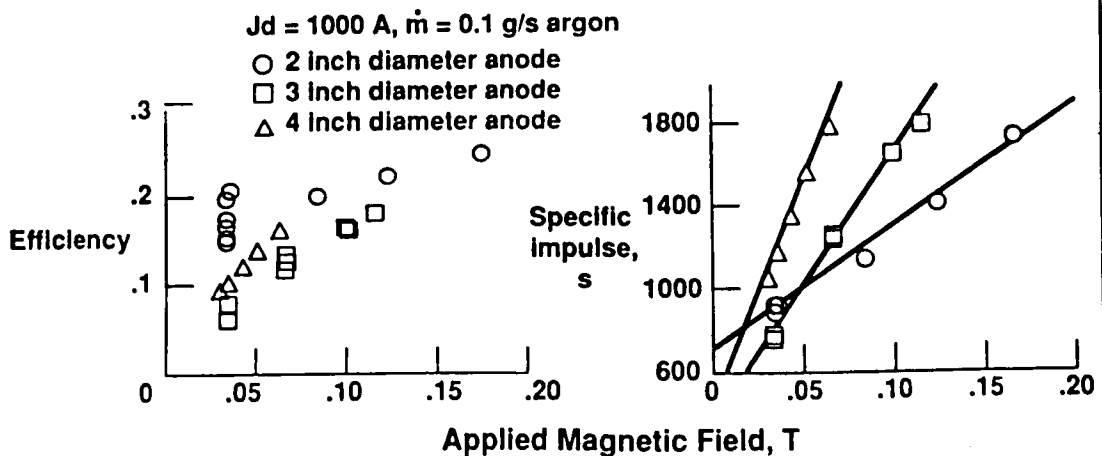
Performance dramatically improved with hydrogen

- Efficiency increased by 2X
- $I_{sp}$  increased by 50%

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MPD Thruster Technology

Thruster Performance  
Geometry and Applied Field Effects

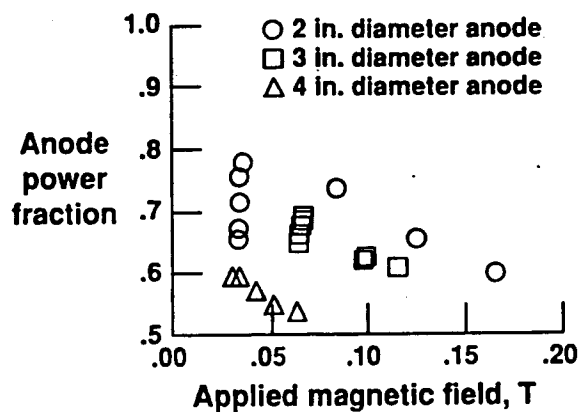


- Efficiency increases with applied field strength
- Specific impulse increases with both anode radius and applied field strength

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**MPD Thruster Technology**

**Anode Power Deposition  
Applied Field and Geometry Effects**



Increasing applied field strength and anode diameter decrease anode power fraction

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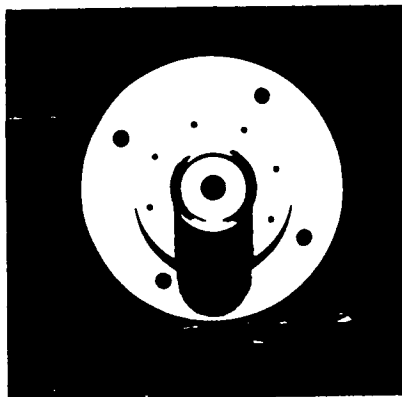
**HIGH POWER ELECTRIC PROPULSION (MPD)**

**MPD THRUSTER HIGH CURRENT  
HOLLOW CATHODE TECHNOLOGY**

High area emitter



Low area emitter



Three hollow cathode assemblies fabricated and prepared for evaluation

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## MPD Thruster Technology

**Scaling Issues**

- Megawatt class operation required for missions of interest
- Cannot operate megawatt class steady-state in current facilities
- Must be able to correlate MW class pulsed thruster operation and steady state data
- Data must enable rational extrapolation to high power levels

How do we realistically study MPD thruster performance and life using currently available facilities?

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## MPD Thruster Technology

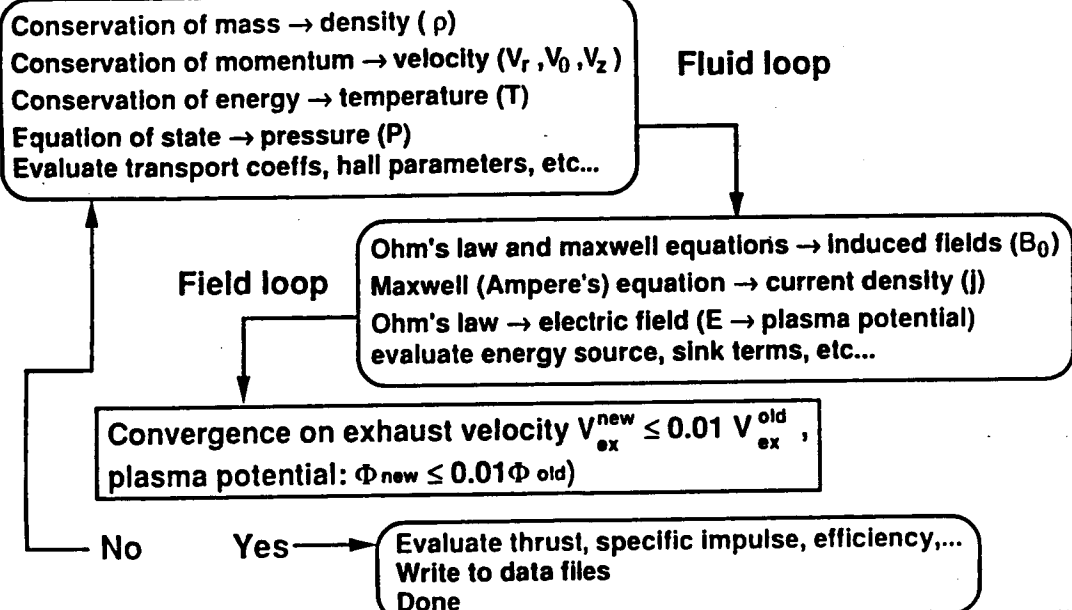
**Diagnostics**

- X-Y probe positioning stand
  - Electrostatic probes
  - enclosed current contours
  - Axial applied B field distribution
- Plume imaging
  - Correlate ion density distribution with applied field
- Spectroscopy
  - Non-invasive temperature and density measurements

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### MPD Thruster Modeling

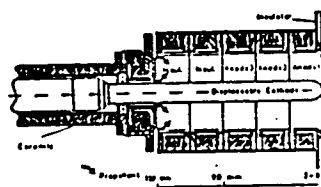
#### Program Outline



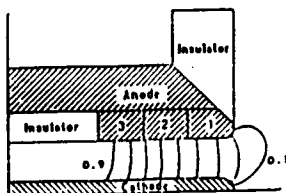
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### MPD Thruster Modeling

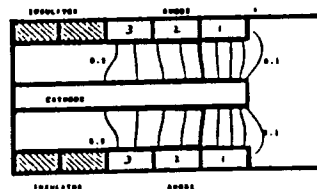
#### Comparison With U. Stuttgart Model/Experiment (6kA, 6 g/s)



Stuttgart-experiment



Stuttgart-model



NASA LeRC-model

#### Current fractions into anode segments

Segment 1:	46%	44%	51%
Segment 2:	27%	27%	22%
Segment 3:	27%	29%	27%

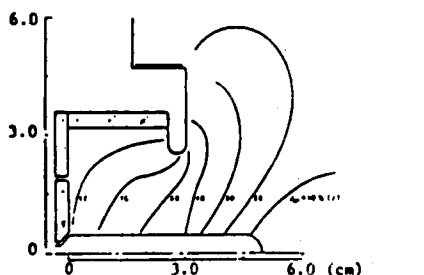
NASA LeRC code in agreement with Stuttgart MPDT experiment/model

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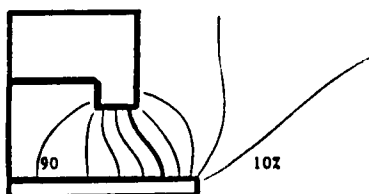
## MPD Thruster Modeling

### Comparison with Princeton University

#### Half-Scale Benchmark Thruster

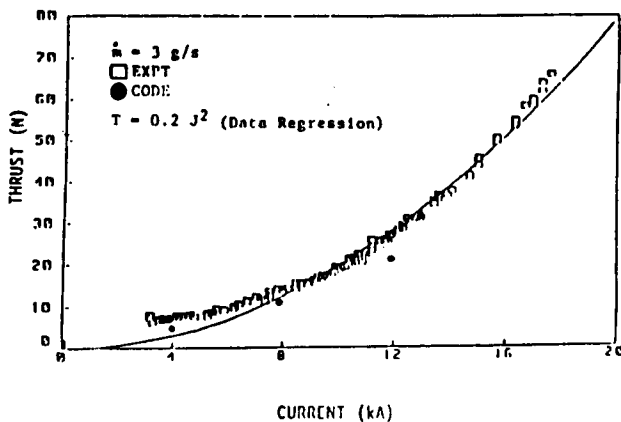


ENCLOSED CURRENT CONTOURS (MEASURED)  
12.4 kA, 1.5 g/s, QUASI-STEADY OPERATION



ENCLOSED CURRENT CONTOURS (PREDICTED)  
12.4 kA, 1.5 g/s, STEADY-STATE OPERATION

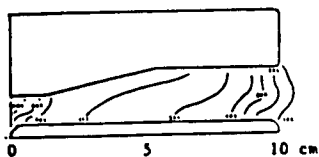
#### Thrust Characteristics



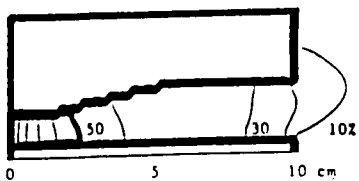
## MPD Thruster Modeling

### Comparison with Princeton University

#### Half-Scale Flared Anode Thruster

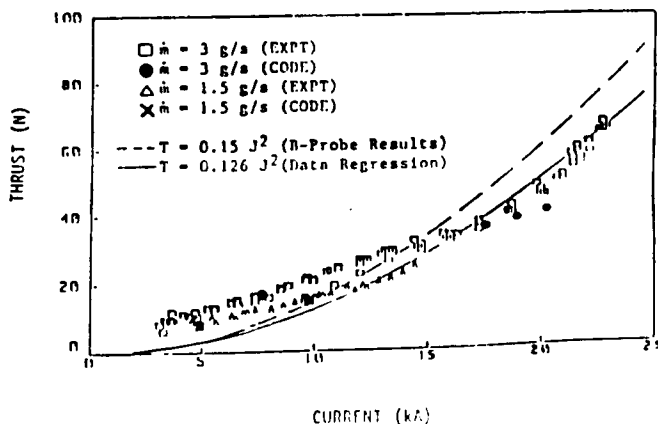


ENCLOSED CURRENT CONTOURS (MEASURED)  
7.9 kA, 3 g/s, QUASI-STEADY OPERATION



ENCLOSED CURRENT CONTOURS (PREDICTED)  
7.9 kA, 3 g/s, STEADY-STATE OPERATION

#### Thrust Characteristics





## **MPD Thruster Modeling**

### **Status**

- Self-field version of MPDT code operational
  - Modest execution times 3-5 hours VAX-CPU)
  - General agreement with experimental results
  - Thruster performance evaluations underway
- Applied-field version of code under development
  - Routines for applied-B distributions incorporated
  - Preliminary testing/modification in progress

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## **KEY TECHNICAL ISSUES**

## KEY SCALING ISSUES

- TWO PRIMARY CONCERNS
  - POWER LEVEL SCALING
  - QUASI-STEADY VS. STEADY STATE
  
- ISSUES MUST BE ADDRESSED USING
  - THEORETICAL MODELS TO ESTABLISH TRENDS AND DEPENDENCIES
  - HIGH FIDELITY PERFORMANCE MEASUREMENTS
  - DETAILED DIAGNOSTICS OF PLASMA AND ELECTRODE PROCESSES USED TO:
    - A. ESTABLISH FUNDAMENTAL RELATIONSHIPS
    - B. VERIFY MODELS

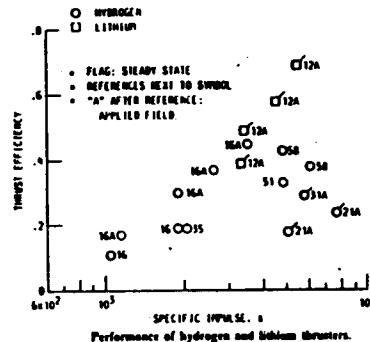
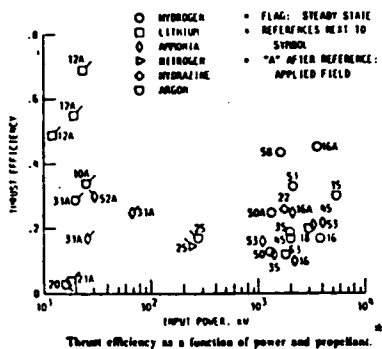
### PERFORMANCE EXPECTATIONS:

- MUST EVALUATE EFFECTS OF :
- PROPELLANT AND APPLIED FIELD
  - ELECTRODE SIZE AND SHAPE
  - PROPELLANT INJECTION

### RELATION BETWEEN QUASI-STEADY AND STEADY-STATE:

- MUST ESTABLISH DATA BASE WITH CORRECT PROPELLANT IN THE APPROPRIATE OPERATING RANGE ( $J^2/\dot{m}?$ )
- MUST MEASURE PERFORMANCE, CURRENT DISTRIBUTIONS, PLASMA AND ELECTRODE PARAMETERS

## PERFORMANCE EXPECTATIONS

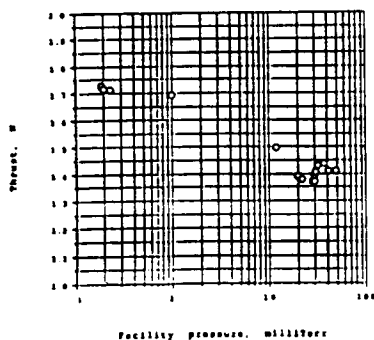


- NOT CORRELATED WITH POWER
- STRONGLY INFLUENCED BY
  - PROPELLANT CHOICE
  - APPLIED OR SELF-FIELD

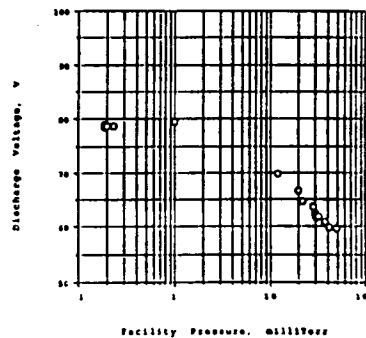
\* Sovey, J. and Manteikis, M. "Performance and Lifetime Assessment of Magnetoplasmadynamic Arc Thruster Technology", J. Propulsion and Power, Vol.7, No. 1, Jan-Feb 1991

## FACILITY REQUIREMENTS

### THRUST



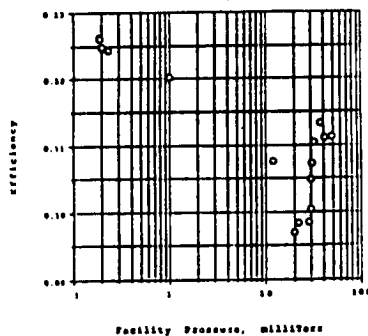
### DISCHARGE VOLTAGE



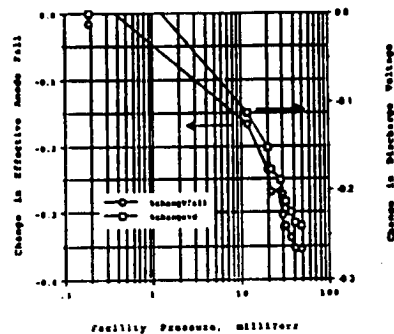
4" D, 3"L ANODE, 0.1 G/S ARGON, 1500 A DISCHARGE,  $B_z = .1$  T

## FACILITY REQUIREMENTS

### EFFICIENCY



### CHANGE IN $V_{an}$ AND $V_d$



Similar anode heat xfer effect observed  
by Saber with self-field thrusters

4" D, 3"L ANODE, 0.1 G/S ARGON, 1500 A DISCHARGE,  $B_z = .1$  T

## POTENTIAL MPDT FACILITIES

FY	FACILITY	THRUSTER POWER, MW		OPERATION TIME, HR	ESTIMATED COST, \$K
		H2	AR		
PRESENT	LERC T5,T6	0.1 (DEM)	0.22 (DEM)	CONT.	-----
1992	LERC T5	0.7-1	1	1 - 2	250 K
1993	LERC T5	1 - 1.5	2	4 - 6	400 K
1995	LERC T6	1 - 1.5	2	'CONT.'	3500 - 5000
1995	LLNL MFTF	1-5		'CONT.'	5000 - 7000
1998	LERC T6	1 - 5	1 - 5	'CONT.'	TBD

## **MATERIAL LIMITATIONS**

### **ANODE:**

- MEASURED HEAT FLUX AT HIGH POWER  $> 5 \text{ KW/CM}^2$  \*
  - LITHIUM HEAT PIPES LIMITED TO  $< 0.5 \text{ KW/CM}^2$
  - OPTIMIZED BEAM DUMP (Cu) LIMITED TO  $\sim 5 \text{ KW/CM}^2$
  - SSME THROAT HEAT FLUX  $\sim 16 \text{ KW/CM}^2$  (relevance?)

### **CATHODE:**

- CURRENT DENSITIES AT HIGH POWER  $> 100 \text{ A/CM}^2$  \*
  - LONG LIFE CATHODES LIMITED TO CURRENT DENSITIES  $\leq 20 \text{ A/CM}^2$  (LOW W.F. TWT CATHODES)

### **INSULATORS:**

- KNOWN TO FAIL AFTER PROLONGED EXPOSURE TO UV AND HIGH TEMPERATURE

- **WE MUST SELECT GEOMETRIES WHERE PERFORMANCE AND ENGINEERING LIMITS CAN BE EVALUATED**

- PRINCETON UNIVERSITY

## **FACILITY LIMITATIONS:**

- MUST MEASURE PERFORMANCE AT PRESSURES  $< 5 \times 10^{-4} \text{ T}$
- FACILITY PRESSURE HAS LARGE EFFECT ON ANODE HEAT XFER, NOT CLEAR ON CATHODE

## **THRUSTER VIABILITY:**

- SHOULD FOCUS ON DEVICES WHICH MATCH ENGINEERING LIMITS FOR:
  - ANODE HEAT TRANSFER
  - CATHODE CURRENT DENSITY
  - INSULATOR LIMITS